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Biocompatible Carbon Nanotube-based Hybrid Microfiber for Implantable Electrochemical Actuator and Flexible Electronic Applications

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KEYWORDS: Hyaluronic acid, Carbon nanotubes, Conductive fiber, Flexible electronics, Electrochemical microactuator, Biocompatibility.

ABSTRACT

Biocompatible, electrically conductive microfibers with superior mechanical properties have received great attention due to their potential applications in various biomedical applications such as implantable medical devices, biosensors, artificial muscles, and microactuators. Here, we developed an electrically conductive and mechanically stable carbon nanotube-based microactuator with low degradability that makes it usable for an implantable device in the

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3 body or biological environments. The microfiber was composed of hyaluronic acid (HA)
4 hydrogel and single-wall carbon nanotubes (SWCNTs) (HA/SWCNT). HA hydrogel acts as
5 bio-surfactant and ion-conducting binder to improve the dispersion of SWCNTs resulting in
6 enhanced electrical and mechanical properties of the hybrid microfiber. In addition, HA was
7 crosslinked to prevent leaking of the nanotubes from the composite. Crosslinking of HA
8 hydrogel significantly enhances Young's modulus, failure strain, toughness, stability of
9 electrical conductivity, and resistance to biodegradation and creep of hybrid microfibers. The
10 obtained crosslinked HA/SWCNT hybrid microfibers show excellent capacitance, and
11 actuation behavior under mechanical loading with the low potential of ± 1 V in a biological
12 environment. Furthermore, the HA/SWCNT microfibers exhibits excellent *in vitro* viability.
13 Finally, biocompatibility is shown through the resolution of early inflammatory response in
14 less than three weeks after implantation of the microfibers in subcutaneous tissue of mice.
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32 **Introduction**

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34 Multifunctional microfibers have been widely researched for various applications including
35 electronic textiles, flexible electronics, artificial muscles, implantable medical devices, and
36 microactuators.¹⁻⁵ Particularly, the development of microfiber-based actuators that can
37 operate in the biological environment in the human body is crucial for biomedical applications
38 such as surgical robots and actuating catheters.⁶⁻⁹ For the realization of microfiber-based
39 actuators, microfibers with reliable mechanical and electrical properties are required. In
40 addition, biocompatibility of microfibers is important for their safe operation in the body,
41 where contact between microfibers and tissues is essential.¹⁰⁻¹³
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54 Conventionally, ionic polymer-metal composites (IPMCs), conducting polymers, and shape
55 memory alloys (SMAs) have been widely used to fabricate microactuators.¹⁴⁻¹⁶ Although
56 IPMCs showed moderate actuation capability, cytotoxicity of the materials hinders their
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3 practical biomedical applications.¹⁷ Conducting polymers are widely used to create various
4 types of microactuators; however, specific dopants and electrolytes with relatively high level
5 of toxicity are required to maintain their unique electrical or electrochemical properties.
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7 SMAAs are typically non-cytotoxic but suffer from low controllability at micro size, long
8 actuator response time, and low energy efficiency.¹⁸ Recently, carbon nanotube (CNT)-based
9 hybrid or composite materials have emerged as promising candidates for the fabrication of
10 microactuators due to their remarkable mechanical and electrical properties in biological
11 environments without using cytotoxic electrolytes.¹⁹⁻²⁴ However, the CNT-based microfiber
12 actuators suffer from creep, short life cycle, and low mechanical stability due to poor
13 interactions between the assembled CNTs. When a mechanical load is applied to CNT-based
14 microfibers, CNTs easily slide with respect to each other due to weak van der Waals
15 interactions between the CNTs.^{25,26} To overcome such behavior, diverse polymeric binders
16 have been utilized. Michardière *et al.* developed microfibers using polyvinyl alcohol
17 (PVA)/CNT hybrid to increase the mechanical stiffness of microfibers. Although Young's
18 modulus of the PVA/CNT hybrid microfibers was twice higher than that of bare CNT
19 microfibers, stretchability under tensile strains significantly decreased.²⁷ Similarly, Lynam *et*
20 *al.* developed chitosan/single walled CNTs (SWCNTs) biofibers, which showed excellent
21 tensile strength (170 ± 46 MPa) and elongation up to break ($6.1 \pm 0.8\%$).²⁸ However, the
22 electrical conductivity of chitosan/SWCNT biofibers was low (1-2 S/cm) due to the poor
23 electrical conductivity of chitosan. DNA/SWCNT biofibers showed improved electrical
24 properties (conductivity: 30 ± 4 S/cm, capacitance: 22.4 F/g), but the elongation of fibers up
25 to break decreased to $3.2 \pm 0.3\%$.²⁹ Despite all the advances to date, there is a lack of highly
26 functional microactuators with the capability to work in the human body without experiencing
27 degradation, fatigue, or creep.

28 To overcome the challenges in the way of fabrication of microactuators for use in human
29 body, hyaluronic acid (HA) is an excellent candidate that acts as biocompatible surfactant and
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3 ion-conducting binder to improve the dispersion of SWCNTs resulting in enhanced electrical
4 and mechanical properties of the hybrid microfiber.³⁰ However, despite high levels of
5 biocompatibility, HA has relatively low viscosity and mechanical stiffness. Furthermore,
6 enzymatic reactions of hyaluronidases in the body can degrade HA. Hence the issues of creep,
7 low fatigue resistance, and degradation of the HA/SWCNT microfibers in biological
8 environments are unresolved. Degradation could also lead to leakage of CNTs to body during
9 *in vivo* operation of the microactuators, which is not desirable. Fabrication of biocompatible
10 microactuators with resistance to creep and degradation remains a challenge and is highly
11 crucial for development of actuators with functionality in biological liquids for implantable
12 and flexible electronics devices.
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28 Here, we addressed the issues of creep, fatigue, degradability, and CNT leakage in
29 HA/SWCNT microactuators with developing chemically crosslinked HA/SWCNT
30 microfibers for biocompatible electrochemical actuators. Our objectives were to design a
31 flexible and mechanically robust SWCNT-based microfiber suitable for applications in the
32 human body by developing a bio-surfactant and ionic-conducting binder that is stable and stiff
33 in biological environments. The effects of SWCNT concentration and crosslinking of HA
34 hydrogel on mechanical properties, conductivity, degradation rate, capacitance, and micro-
35 actuation behavior of HA/SWCNT hybrid microfibers were comprehensively investigated.
36 Finally, we conducted *in vitro* cell growth experiments on the surface of the microfibers and
37 *in vivo* implantation of microfibers to evaluate the cytocompatibility and biocompatibility of
38 the microactuators.
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54 **Experimental Section**

55 **Fabrication of HA/SWCNT microfibers**

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3 HA/SWCNT microfibers were fabricated using wet spinning technique. The weight ratio of
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5 HA (Lifecore Biomedical LLC, MW: 41 KDa – 65 KDa) to SWCNTs (NanoIntegris
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7 Technologies Inc.) in suspension was optimized to produce uniform and well-dispersed
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9 solutions, and 5: 8 was chosen as the optimum ratio, which is close to those reported in
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11 literature.³¹ HA solutions with different concentrations (1, 2.5, 3.125, 3.75, 4.375 mg/mL)
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13 were prepared by dissolving HA in de-ionized (DI) water at room temperature. Then,
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15 SWCNTs were added and dispersed in the solution for 20 minutes using a probe sonicator
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17 (Qsonica Sonicator, Newton, USA). The SWCNTs were uniformly dispersed in the HA
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19 solution (Figure S1). To obtain microfibers, the homogeneous HA/SWCNT dispersion was
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21 injected into a rotating coagulation bath (5% CaCl₂ in 70% ethanol, 20 rpm) through a 0.2
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23 mm diameter syringe needle with 50 mL/h flow rate. The coagulated HA/SWCNT
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25 microfibers were taken out from the coagulation bath, washed with ethanol, and dried in order
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27 to remove the remaining coagulating agents. To crosslink the HA hydrogel, the coagulated
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29 microfibers were immersed in hexamethylenediamine (HMDA) solution for 1 hr and washed
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31 with ethanol.³² Then, the crosslinked microfibers were placed into an aqueous solution of 1-
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33 Ethyl-3-[3-(dimethyl amino)propyl]carbodiimide (EDC) (5.4 mg/mL) and 1-
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35 hydroxybenzotriazole monohydrate (HOBt) (3.8 mg/mL) for 10 minutes, to activate the
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37 carboxyl groups within the structure of HA. To complete the reaction, HMDA was added to
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39 the solution, and the solution was then incubated at 37° C for 1 hr. The molar ratio of HMDA
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41 to the carboxyl group of HA was 1:1. The obtained HA/SWCNT microfibers were then dried
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49 in air.
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52 **Characterization of the dispersion of HA/SWCNT suspension**

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54 Homogeneity of the HA/SWCNT dispersion was assessed with 3D digital microscopy (DSX-
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56 CB, Olympus Ltd., Japan), scanning electron microscopy (SEM) (S-4700, Hitachi Ltd., Japan)
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58 and field emission high resolution transmission electron microscopy (HR-TEM) (Tecnai G2,
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3 FEI, USA). After ultrasonication, for optical imaging, drops of the HA/SWCNT suspension
4 were placed on a glass slide for microscope imaging. For SEM imaging, drops were placed on
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6 SEM stubs, dried for 24 h in air, and sputter coated with gold for 1 minute prior to
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8 examination in SEM with an operating voltage of 10 kV. For TEM imaging, a 10 μ L drop of
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10 the HA/SWCNT suspension was first diluted in 10 mL of distilled water, then placed on a
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12 copper grid to image using 80 kV operating voltage.
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18 **Characterization of the structure of HA/SWCNT microfibers**

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20 The morphology and microstructure of HA/SWCNT microfibers were characterized using
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22 SEM. The surface roughness of microfibers was probed by an atomic force microscope (AFM,
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24 Bruker AXS, German) in tapping mode. The Raman spectra were measured using a Raman
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26 spectrometer (XploRA, HORIBA Jobin Yvon, France) with an excitation wavelength of 532
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28 nm and a laser power of 1 mW. Fourier transformed infrared spectroscopy (FTIR, Nicolet
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30 is50, Thermo Fisher Scientific, USA) was used to confirm the functional groups present in the
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32 uncrosslinked and crosslinked HA/SWCNT microfibers. The fibers were cut into small pieces
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34 and were grinded with KBr. Then, the powder was pressed by tablet press for 20 s and was
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36 tested at room temperature.
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43 **Degradation testing of HA/SWCNT microfibers**

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45 Degradation of the HA/SWCNT microfibers was tested by placing microfibers with equal
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47 weight in closed bottles containing Dulbecco's phosphate-buffered saline (DPBS) (2 mL) and
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49 hyaluronatylase (50 U) at 37°C. HA digestion was monitored by measuring the absorbance
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51 values from the DPBS supernatant (2 μ L) at a wavelength of 260 nm using a plate reader
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53 (NanoDrop 1000, Thermo Scientific). Three samples for each condition were tested, and the
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55 average value of absorbance was calculated.
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Mechanical characterization of HA/SWCNT microfibers

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3 The mechanical properties of HA/SWCNT fibers were determined using a uniaxial
4 mechanical tester (Instron, Norwood, USA) in a tensile mode. The ends of the HA/SWCNT
5 microfibers were fixed on a 2 cm paper frame by applying a superglue. For wetting the dry
6 HA/SWCNT fibers, we sprayed the fibers and allowed them to swell for 5 minutes before
7 testing. The stress-strain curves were plotted up to the point of failure of the microfibers.
8 Young's modulus was measured as the slope of the linear region of the stress-strain curve.
9 Tensile strength and failure strain were determined using the maximum stress and strain at the
10 point of failure, respectively. Toughness was calculated as the area under the stress-strain
11 curve. Average values of the properties measured for at least three specimens for each sample
12 condition were reported.
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28 **Electrical characterization of HA/SWCNT microfibers**

29 The electrical conductivity of the HA/SWCNT microfibers was measured by four-point probe
30 method for a minimum of three fibers for each condition. A constant current of 1 mA was
31 applied through the outer electrodes using a source meter (B2900 Series, Agilent, USA) and
32 the voltage difference was measured between the two inner electrodes after 10 s using a
33 digital multimeter (34401A, Agilent, USA). Silver paste was used at the contacting points
34 between the fiber and the electrode probes in order to eliminate contact resistance. The
35 diameters of the microfibers were measured using microscope images and the conductivity (σ)
36 was calculated using Equation (1):
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$$48 \quad \sigma = (L \times I) / (S \times V) \quad (1),$$

49 where S is the cross-sectional area of the HA/SWCNT microfibers, L is the length between
50 the two inner points, V is the voltage across the two inner probes, and I is the constant current
51 applied to the fibers.
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59 **Electrochemical capacitance of HA/SWCNT microfibers**

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3 CV curves were recorded to measure the capacitance of HA/SWCNT microfibers using an
4 electrochemical workstation (Model 600E Series, CH Instruments, USA). A three-electrode
5 electrochemical cell was used for the CV tests. The HA/SWCNT microfiber, an Ag/AgCl
6 electrode, and a Pt electrode were used as the working electrode, reference electrode, and
7 counter electrode, respectively. The electrochemical capacitance of HA/SWCNT microfibers
8 was measured from the CV curves obtained within the potential window of -1 to 1 V with 25-
9 100 mV/s scan rate in the DPBS solution. The HA/SWCNT microfibers were held in the
10 DPBS for 30 mins before the tests.
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23 **Characterization of the actuation behavior of HA/SWCNT microfibers**

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25 The actuation behavior of HA/SWCNT microfibers was tested by using Muscle Lever Arm
26 System (300C-LR, Aurora Scientific Inc., Canada) combined with the electrochemical
27 workstation. The microfibers were held vertically in the electrolyte solution; the bottom end
28 of the microfiber firmly clamped to the electrochemical workstation by Pt wire, and the top
29 end of the microfiber was fixed on the strain sensor in the lever arm system by silicone epoxy
30 glue. Then the microfiber was immersed in the DPBS solution for 2 hrs under an applied
31 tensile force of 4 mN to equilibrate. The applied potential changed between -1 and +1 V with
32 a scan rate of 25 mV/s. The actuation strain due to expansion/contraction of the fiber was
33 calculated using:
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$$46 \text{ Strain (\%)} = ((I - I_0) / I_0) \times 100 \quad (2),$$

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48 where I and I_0 represent the instantaneous and original length of the microfiber, respectively.
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52 **Evaluation of the *in vitro* cytocompatibility of HA/SWCNT microactuators**

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54 To test cell compatibility, 1×10^6 NIH-3T3 fibroblasts were cultured on HA/SWCNT
55 microfiber using standard cell culture protocols. Cells were seeded directly on the surface of
56 the microfibers after sterilization of the samples using ultraviolet light. High glucose
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3 Dulbecco's Modified Eagle Medium (DMEM) supplemented with 10% fetal bovine serum
4 (FBS) and 1% penicillin-streptomycin was used as medium to culture cells at 37° C and 5%
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6 CO₂. Cell viability was evaluated using a Live/Dead assay kit (calcein-AM/ethidium Bromide
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8 homodimer, Invitrogen) according to the manufacturer's instructions. The viability of cells
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10 was calculated using Image J software based on counting the number of live and dead cells
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12 and then dividing them by total cell number. Immunocytochemistry of the fibroblast cells was
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14 performed after 5 days of cell culture. The cells seeded on the microfibers were fixed using 4%
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16 formaldehyde for 1 hr at room temperature, followed by incubation in 0.1% Triton X-100 for
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18 30 minutes, and washing 3 times with the DPBS. Then, the fibers were incubated with Alexa
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20 Fluor 488-phalloidin and DAPI to stain the F-actin and cell nuclei as described in the
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22 manufacturer's instruction. The fluorescence images were captured using an inverted
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24 microscope (Nikon, Eclipse TE 2000U, Japan).
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32 ***In vivo* implantation of HA/SWCNT microfibers for evaluation of biocompatibility**

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34 Six-week-old, female mice (C57 BL/6, Orientbio, Seoul, Korea) were anaesthetized with
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36 xylazine and ketamine. Uncrosslinked and crosslinked HA/SWCNT microfibers were
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38 implanted into the dorsal subcutaneous spaces of mice (n = 4 per group). After one and three
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40 weeks, the implanted HA/SWCNT microfibers were retrieved, fixed in 4% (v/v)
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42 paraformaldehyde (PFA), embedded in paraffin, and sectioned transversely into 6- μ m-thick
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44 sections. For histological analysis, the prepared sections were stained with Hematoxylin
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46 (Sigma-Aldrich) and Eosin (Sigma-Aldrich) staining and rinsed with distilled water for
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48 microscopy analyses of the implanted area. For immunohistochemical analysis, prepared
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50 sections were deparaffinized and hydrated by sequential incubations in xylene and ethanol.
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52 After being washed with the DPBS for 2 minutes, the sections were pre-blocked with 3%
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54 H₂O₂ for 10 minutes. Following incubation with the primary antibody against CD68 (Abcam)
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56 and CD86 (Abcam) for 1 hr at room temperature, the sections were incubated with Alexa
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3 Fluor 488 goat anti-mouse antibody and Texas Red goat anti-rabbit antibody (Applied
4 Biological Materials Inc). Fluorescence images were captured using a Nikon microscope
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6 Eclipse 55i (Nikon, Kanagawa, Japan).
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10 11 12 **Statistical analysis**

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14 Statistical significance was evaluated by performing one-way ANOVA tests (GraphPad Prism
15 5.02, GraphPad Software). To analyze and assess significant differences between selected
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17 treatments, Tukey's multiple comparison tests were utilized. Differences were characterized as
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19 significant for $*p < 0.05$, $**p < 0.01$, and $***p < 0.001$.
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27 28 **Results and Discussion**

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30 We fabricated HA/SWCNT microfibers using a motorized wet-spinning method. The
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32 motorized wet-spinning system was composed of a syringe pump for the injection of
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34 HA/SWCNT suspension and an automatic rotator for rotation of the coagulation bath (Figure
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36 1a). Microfibers were produced by spinning of HA/SWCNT suspension in CaCl_2 as
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38 coagulation bath. The liquid suspension is solidified in the coagulation bath through a
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40 combination of inter- and intra-chain ionic crosslinking and solvent-induced fiber formation.
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42 Upon injection of the HA/SWCNT suspension into the CaCl_2 coagulation bath, calcium ion
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44 physical crosslinking of HA chains through D-glucuronic acid residues occurs.³⁰ After fiber
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46 formation, we took the wet-spun fibers out of the coagulation bath and dried them at room
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48 temperature with stretching forces to further align the SWCNTs along the fiber axis. The
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50 produced fibers are meter-scale long and have circular cross-sections with a constant diameter
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52 along the entire length (Figure 1b,c), which is precisely controllable by the injection rate of
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54 the ink and the rotation rate of the rotor. Using a suspension solution composed of SWCNTs
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56 and HA (1.6:1 weight ratio) in water, an injection rate of 50 mL/h and a rotation rate of 20
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rpm, the fibers had an approximate diameter of 50 μm at dry state (Figure 1c-(i)). Due to the shear force in the process of solution injection and coagulation, the surface showed nanoscale roughness along the microfibers (Figure 1c-(ii)).

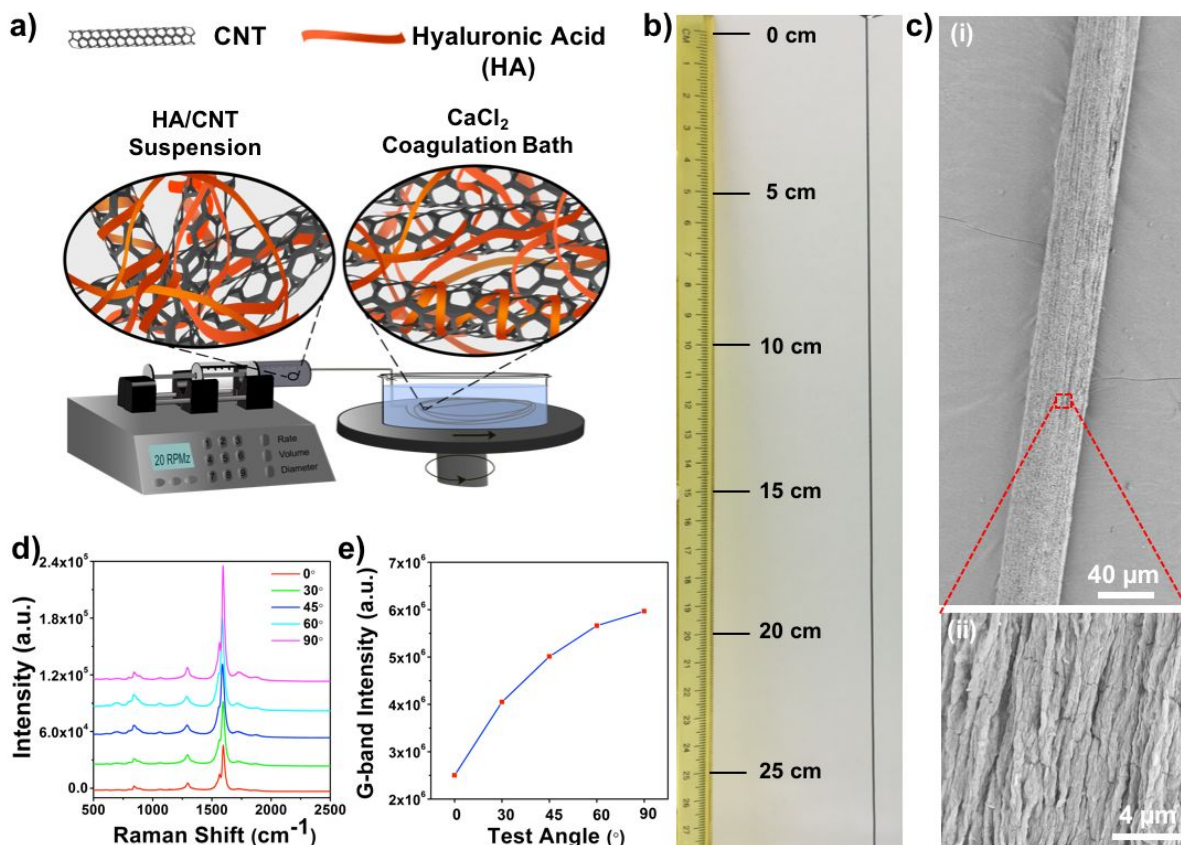


Figure 1. a) Schematic illustration of the wet spinning set up for the fabrication of HA/SWCNT hybrid microfibers with 4 mg/mL SWCNT concentration. b) Photograph of a long HA/SWCNT microfiber fabricated in the wet spinning process. c) SEM images of a dried HA/SWCNT microfiber at (i) low and (ii) high magnifications. d) Polarized Raman spectra of an HA/SWCNT microfiber with the fiber axis at 0°, 30°, 45°, 60° and 90° with respect to the excitation polarization direction. (e) G-band peak intensities as a function of the angle between the fiber and the excitation polarization axis.

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3 The orientation and alignment of SWCNTs within the HA/SWCNT microfibers were
4 further characterized using polarized Raman spectroscopy. Evaluation of the intensity of the
5 laser beam upon the change of the polarization axis of the electric field in the laser beam with
6 respect to a reference axis shows the degree of anisotropy within a composite material.³³ With
7 the change of electric field axis from perpendicular (90°) to parallel (0°) to the HA/SWCNT
8 microfibers, the beam intensity is increased, confirming the structural anisotropy of the
9 HA/SWCNT microfibers (Figure 1d).³⁴ The maximum G-band intensity, which is a
10 qualitative indication of the orientation of SWCNTs, is gradually increased as the angle
11 between the incident beam and fiber axis is increased. The increase in the maximum G-band
12 intensity indicates that SWCNTs are highly aligned within the fibers along with the direction
13 of the fiber axis (Figure 1e).³⁵

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HA is a naturally-occurring biomolecule in the human body and has been widely used for
various biomedical applications such as drug delivery and tissue engineering.³⁶ However, it is
highly degradable in body through the enzymatic reactions of hyaluronidases. The chemical
modification of HA is a reliable way to improve its degradation performance. HA derivatives
not only maintain the original characteristics such as biological compatibility and cell
adhesion, but also provide a series of other excellent features such as mechanical strength,
viscosity, resistance to hyaluronidase degradation and targeting characteristics.³⁷ HA
derivatives have been widely used in tissue engineering, drug delivery, wound healing, and
devices in several surgical procedures.^{38,39} The three most commonly used chemical
modification sites in HA are carboxylic groups, hydroxyl groups, and $-\text{NHCOCH}_3$ groups
(Figure S2). Carboxylic groups have a higher level of activity and are the receptors of HA or
hyaluronidase identification points. Therefore, carboxylic groups were chosen as the target for
modification to minimize the biodegradation of HA. In this paper, HMDA was used as a
chemical crosslinker of HA (Figure 2a). Wet-spun fibers were placed in an aqueous solution
of EDC and HOBt to activate the carboxyl groups in the backbone of HA biomolecules.

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3 HMDA was then added to crosslink HA chains by chemical bonding between the amide and
4 carboxyl groups.³² Figure S2 displays a schematic representation of HA crosslinked with
5 HMDA after activation using EDC and HOBt. The crosslinking of HA in SWCNT
6 microfibers was confirmed by FTIR spectroscopy, SEM, AFM, Raman, degradation test and
7 tensile test. Comparing with SWCNTs, both uncrosslinked and crosslinked HA/SWCNT
8 microfibers show a broad absorption peak at 3600 cm^{-1} - 3000 cm^{-1} and absorption peaks at
9 3000 cm^{-1} - 2800 cm^{-1} in Figure S3 due to the O-H and C-H stretching vibrations in HA,
10 respectively.⁴⁰ Several highly overlapped bands also exist in the spectrum for uncrosslinked
11 and crosslinked HA/SWCNT microfibers. The overlapped band at 1633 cm^{-1} is assigned to
12 the C=O stretching of amide I band coupled with N-H bending in the GlcNAc unit and the
13 antisymmetrical stretching mode of the carboxylate group in the GlcA unit.^{41,42} The peak was
14 shifted to 1635 cm^{-1} and absorption intensity increased for crosslinked HA/SWCNT
15 microfibers due to the overlapped absorption of N-H bending in HMDA and N-H acetamide
16 groups in HA. Moreover, the intensity of the absorption band at 1384 cm^{-1} - the result of
17 overlapped C-O stretching and N-H bending vibration of Amide III band - was increased by
18 the introduction of N-H vibration due to the crosslinking reaction. The peak at 1405 cm^{-1}
19 represents the C-O-C stretching vibration in HA/SWCNT microfibers and was slightly shifted
20 to 1407 cm^{-1} after the crosslinking reaction, which is in agreement with a previous study on
21 HA/HMDA hybrid hydrogels.⁴³ Figure 2b-(i), (ii) show the SEM images of nanofibrous
22 networks at the fractured cross sectional areas of HA/SWCNT microfibers before and after
23 crosslinking. The cross-sectional images of the crosslinked fibers show more winding and
24 tangled nanofibrous networks compared to the uncrosslinked fibers with straighter and less
25 tangled ones. Furthermore, morphological profiles from AFM images revealed rougher
26 surfaces of the crosslinked microfibers than the uncrosslinked microfibers, which is a result of
27 the formation of networks due to HA chemical crosslinking (Figure S4). The effect of
28 chemical crosslinking on the nanostructure of the HA/SWCNT microfibers was evaluated
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3 using Raman Spectroscopy. In a typical Raman spectrum of CNTs, the D band peak indicates
4 the structural defect mode, which is attributed to disordered carbon (defects and amorphous
5 carbon), while the G band peak indicates the stretching mode in the graphene plane. A lower
6 D/G peak ratio indicates that the microfiber has fewer defects and a higher degree of graphitic
7 crystallinity.⁴⁴ The D/G ratios measured for the microfibers do not show a significant
8 difference between the uncrosslinked (0.18 ± 0.01) and crosslinked HA/SWCNT microfibers
9 (0.17 ± 0.02) (Figure 2c). Thus, the obtained Raman spectra suggest that the HMDA
10 treatment does not damage the nanostructure of the SWCNTs within the microfibers.

11
12 Degradation of HA hydrogel was characterized by placing the HA/SWCNT microfibers
13 and hyaluronidase (25 U/mL) in the DPBS for 5 days. Due to the enzymatic reactions of
14 hyaluronidase, the color of DPBS turns dark for the uncrosslinked microfibers. The
15 dissolution of HA hydrogel was not observed in the crosslinked microfibers (Figure 2d). HA
16 hydrogel digestion was analyzed by measuring the absorbance values of the DPBS
17 supernatant at 260 nm wavelength, which is the characteristic absorption peak of SWCNTs,
18 over 175 hrs after hyaluronidase treatment. A significant difference was observed between the
19 crosslinked and uncrosslinked microfibers, showing minimal degradation of HA hydrogels in
20 the crosslinked microfibers (Figure 2e); the absorbance value in the case of supernatant taken
21 from the vial containing uncrosslinked HA/SWCNT microfibers was 0.38 after 120 hrs,
22 which was an order of magnitude higher than the value in the case of crosslinked
23 HA/SWCNT microfibers (0.03). The carboxyl groups within the structure of HA have known
24 targets for hyaluronidase in the process of HA degradation.^{45,46} Therefore, the lower amount
25 of degradation of the crosslinked microfibers provides evidence for the modification of
26 carboxyl groups due to crosslinking with HMDA. The crosslinked HA/SWCNT microfibers
27 are expected to be more stable in the body with the presence of hyaluronidase. Furthermore,
28 we measured mechanical properties of the microfibers before and after the HA hydrogel
29 digestion test (Figure 2f). After the degradation test, Young's modulus and tensile strength
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were, respectively, on average 75% and 600% higher for the crosslinked HA/SWCNT microfibers compared to the uncrosslinked ones. The durable mechanical integrity of crosslinked fibers in the hyaluronidase-containing liquid is well matched with the application as actuators in biological settings.

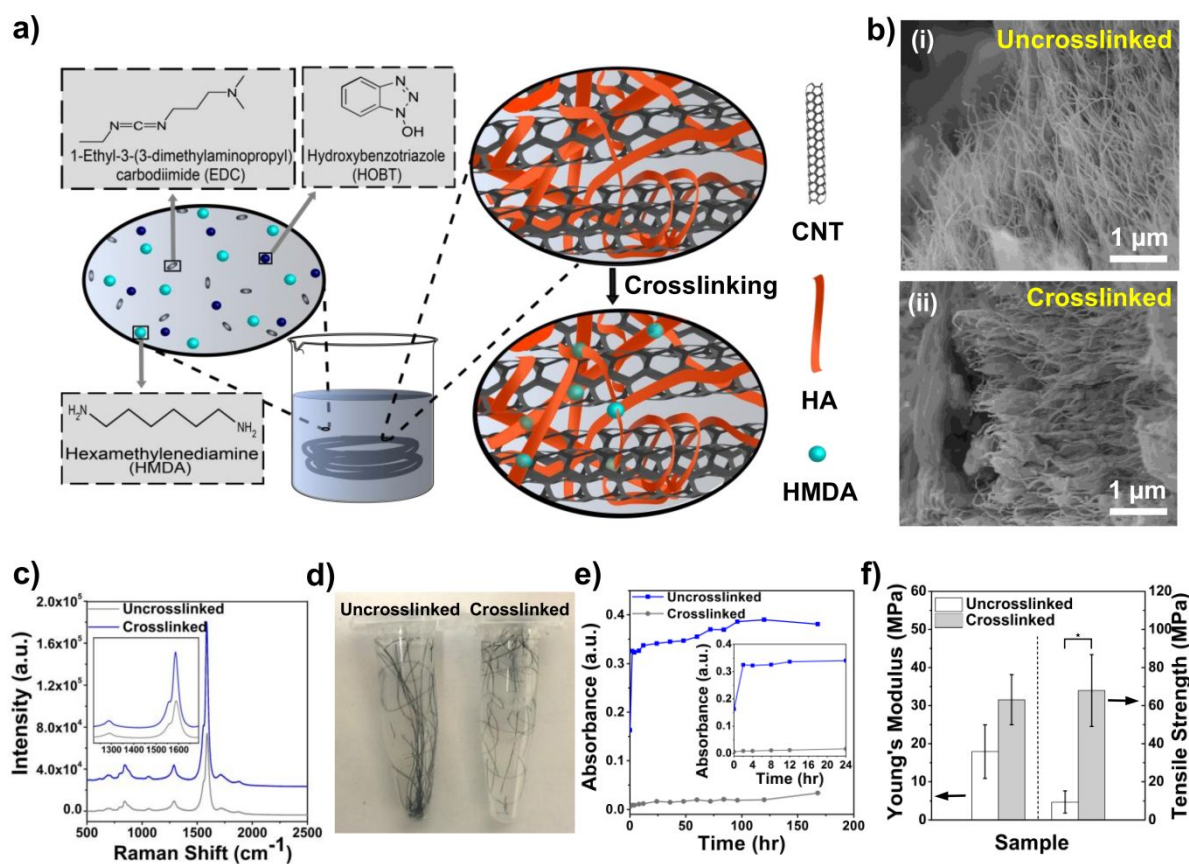


Figure 2. Crosslinking of HA within the HA/SWCNT microfibers with 4 mg/mL SWCNT concentration. a) Schematic illustration of the crosslinking process of HA/SWCNT microfibers. b) Cross-sectional SEM images of (i) uncrosslinked and (ii) crosslinked HA/SWCNT microfibers. c) Polarized Raman spectra of uncrosslinked and crosslinked HA/SWCNT microfibers. d) Photographs of HA/SWCNT microfibers in the DPBS and hyaluronidase to evaluate the degradation of HA/SWCNT microfibers. e) Absorbance at 260 nm measured from the DPBS supernatant containing HA/SWCNT microfibers and hyaluronidase. f) Tensile strength and Young's modulus of crosslinked and uncrosslinked

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3 HA/SWCNT fibers after 5 days storage in the DPBS and hyaluronidase. Results are presented
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5 as means \pm standard deviations ($n = 3$; * $p < 0.05$, ** $p < 0.01$, and *** $p < 0.001$).
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11 Uniaxial tensile testing of swollen fibers to the point of fracture enabled comparison of the
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13 mechanical properties of HA/SWCNT microfibers with and without chemical crosslinking
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15 and as a function of SWCNT concentration (Figure 3). Figure 3a shows representative stress-
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17 strain curves of HA/SWCNT microfibers at 6 mg/mL SWCNT concentration with and
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19 without chemical crosslinking. Two stages of deformation could be identified from the stress-
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21 strain curves. First, HA/SWCNT microfibers showed linear relationship between stress and
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23 strain, suggesting an initial elastic deformation during stretching. The stress in this stage is
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25 carried by both CNT and HA with reversible stretching as the dominant mode of deformation.
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27 Then, stress within the HA/SWCNT microfibers increased nonlinearly to the point of failure
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29 of the microfibers. Irreversible sliding and slippage of CNTs and HA chains are the cause of
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31 larger deformations in this stage, whereas the stress is probably carried mainly by HA chains.
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33 Failure strain – the engineering strain at the point of fracture of HA/SWCNT microfibers –
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35 increased with chemical crosslinking of HA and with increasing the SWCNT concentration in
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37 both the uncrosslinked and crosslinked HA/SWCNT microfibers (Figure 3b). By increasing
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39 the SWCNT concentration from 4 to 8 mg/mL, the failure strain increased from $2.0 \pm 0.6\%$ to
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41 $6.1 \pm 1.6\%$ for uncrosslinked microfibers and from $4.9 \pm 0.4\%$ to $11.7 \pm 2.6\%$ for crosslinked
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43 ones. The Young's modulus and tensile strength increased dramatically with both chemical
44
45 crosslinking of HA and increasing the SWCNT concentration up to 7mg/mL (Figure 3c and
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47 Figure S5). The Young's modulus increased from 0.5 ± 0.1 GPa for 4 mg/mL uncrosslinked
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49 HA/SWCNT microfibers to 1.8 ± 0.4 GPa for 7 mg/mL crosslinked HA/SWCNT microfibers.
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51 The improvement of mechanical properties as the result of crosslinking is related to the
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53 formation of polymeric networks through covalent bonding of HA chains, which improve
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3 load transfer between adjacent CNTs. Significantly larger forces are required for the
4 deformation of a chemically bonded network of polymeric chains than physically crosslinked
5 chains (Figure 3d). Furthermore, the covalently crosslinked structure undergoes higher
6 magnitudes of elongation before break, compared to the case of looser chains (Figure 3d).
7
8 Crosslinking of HA hydrogel improved the interfacial interaction between the SWCNTs and
9 HA network, hence resulting in preferable mechanical interlocking of SWCNTs within
10 microfibers; stress is transferred more effectively between the HA hydrogel and the SWCNTs.
11
12 SWCNTs function as load-bearing components of the hybrid structure to contribute to the
13 stiffness and strain. Therefore, the mechanical properties of the HA/SWCNT microfibers
14 exhibited an ascending trend with an increase in SWCNT and HA concentration, due to the
15 increase in the density of the load-bearing SWCNT components. However, when the SWCNT
16 concentration increased to 8 mg/mL, Young's modulus and tensile strength of crosslinked
17 HA/SWCNT microfibers decreased to 1.0 ± 0.5 GPa. Such a decrease may be attributed to the
18 poor distribution of SWCNTs in the microfibers and weak interactions between SWCNT
19 agglomerations, which reduce the resistance to deformation of HA/SWCNT microfibers. The
20 change in Young's modulus of uncrosslinked fibers with increasing SWCNT concentration is
21 not significant, due to the fact that SWCNTs are less effective load-bearing components of the
22 hybrid structure in an uncrosslinked HA hydrogel than in crosslinked one, hence decreasing
23 the influence of SWCNT concentration on Young's modulus (Figure S6). The combination of
24 increase in failure strain, stiffness, and strength translates to tougher microfibers through
25 chemical crosslinking; toughness increases significantly, as determined by the extent of the
26 area under stress-strain curves (Figure 3e). The hierarchical porous structure of the microfiber
27 experiences higher magnitude of energy absorption before break, which is an outstanding
28 advantage for application as an actuator. In addition to the role as load-bearing constituents of
29 the microfibers, SWCNTs play a role in the enhanced toughness by bridging the micro- and
30 nano-scale cracks (SWCNT pull-out; Figure 3f(i), (ii)) to increase fracture toughness and
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3 improve energy absorption. No particular trend exists in the toughness vs. SWCNT
4 concentration due to the different trends in the failure strain and Young's modulus. The
5 highest magnitudes of toughness correspond to the SWCNT concentrations of 5 and 7 mg/mL.
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7 The combination of trends observed in failure strain, Young's modulus, and toughness shows
8 that 7 mg/mL is the SWCNT concentration resulting in optimum mechanical properties.
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10 We characterized the electrical properties of HA/SWCNT microfibers with different
11 SWCNT concentrations (Figure 3g), as electrical characteristics relate directly to the
12 performance of electrochemical actuators. For the uncrosslinked HA/SWCNT microfibers, the
13 resistivity decreased from $1.7 \times 10^{-4} \pm 5.5 \times 10^{-5} \Omega \cdot \text{m}$ to $9.1 \times 10^{-5} \pm 1.2 \times 10^{-5} \Omega \cdot \text{m}$ as SWCNT
14 concentration varied from 4 mg/mL to 8 mg/mL. The decrease of resistivity is mainly due to
15 the formation of more electrical pathways with increasing the amount of electrically
16 conductive SWCNTs. Crosslinking of HA hydrogel increased resistivity; the increase in
17 resistivity by crosslinking is attributed to the addition of the insulating crosslinker - HMDA -
18 to the network of HA-coated SWCNTs and formation of a porous structure with the networks
19 of HA/SWCNT (Figure 2b and Figure S4) because of chemical crosslinking. Such a porous
20 structure decreases the number of direct contact points between the SWCNTs, resulting in
21 lower number of existing electrical conductive pathways. Notably, the magnitude of increase
22 in resistivity was significantly higher at the lowest and the highest SWCNT concentrations.
23 We speculate that the highest resistivity at 4 mg/mL is related to the SWCNT density (Figure
24 S7) being lower than the percolation threshold required for the formation of current flow
25 pathways. The second highest resistivity at 8 mg/mL is due to the SWCNT agglomerations.
26 SEM shows the lower density at 4 mg/mL, as evident from larger pores and less compact HA-
27 wrapped SWCNTs (Figure S7). The SWCNT agglomerations are distinguishable in both
28 optical microscopy images of HA/SWCNT solutions (Figure S8a) and SEM images of
29 microfibers (Figure S8b). Optical microscopy images of HA/SWCNT dispersion (Figure S8a)
30 show no particles greater than 3 μm in size in the 7mg/mL HA/SWCNT suspension, but 8
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3 mg/mL HA/SWCNT suspension contained visible agglomerations ($5\mu\text{m} \sim 15\mu\text{m}$). When the
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5 HA/SWCNT suspension was assembled into microfibers, these agglomerations created rough
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7 surfaces of the 8 mg/mL SWCNT concentration microfibers while HA/SWCNT microfibers
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9 with 7 mg/mL SWCNT concentration had a more uniform and smoother surface (Figure S8b).
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11 Thus, we speculate that the conductivity of HA/WCNTs microfibers were adversely affected
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13 by the agglomerations. Therefore, for the crosslinked microfibers, the best electrical
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15 performance occurs between 5-7 mg/mL SWCNT concentration.
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19 Although chemical crosslinking of HA hydrogel increases electrical resistance, the
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21 favorable mechanical properties of the crosslinked microfibers are expected to affect their
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23 electrical conductance during actuation. To investigate the change of electrical characteristics
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25 during mechanical loading, we evaluated electrical resistivity normalized by the original
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27 resistivity (R/R_0) in three modes of mechanical loading: tensile, sharp bending, and cyclic
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29 folding (i.e. fatigue testing). The bending and cyclic loading resemble high strain and repeated
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31 loading during application as actuators. Microfibers were attached to a paper with the two
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33 ends of the microfibers connected to copper wires using conducting silver paste in all three
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35 tests. Stress-strain behavior and the corresponding resistivity in tensile loading revealed a
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37 near-linear increase for both uncrosslinked and crosslinked HA/SWCNT microfibers in
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39 resistivity with strain (Figure 3h). The increase in resistivity is a consequence of tensile strain
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41 in the material, which weakens the SWCNT junction contact points and breaks some of the
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43 electrical pathways. The crosslinked HA/SWCNT microfibers were less significantly affected
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45 by strain due to stronger SWCNT junction contact points and more stable electrical pathways.
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47 The increase in resistivity is higher for the case of uncrosslinked microfibers than crosslinked
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49 ones, as measured by bending the fiber attached to a paper substrate (Figure 3i and Figure S9);
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51 the uncrosslinked HA/SWCNT microfibers showed, on average, 11% increase in resistivity
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53 while the crosslinked samples showed 6%, revealing higher stability of crosslinked
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55 HA/SWCNT microfibers in large bending angles. The stability of the electrical conductance
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3 was further examined in cyclic mechanical deformations by folding-unfolding cycles
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5 performed on the microfiber using a mechanical tester and simultaneous measurement of
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7 resistivity (Figure 3j and Figure S10). The resistivity of crosslinked HA/SWCNT microfibers
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9 remained within 10% increase in magnitude over 2500 cycles and reached a plateau of
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11 approximately 14% increase at 3000 cycles. However, the resistivity of uncrosslinked
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13 HA/SWCNT microfibers was increased significantly faster during folding cycles and reached
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15 approximately 65% increase at 3000 cycles. Crosslinking produces chemically bonded HA
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17 networks and enhanced interlocking of SWCNTs and HA, which reduce the number of micro-
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19 and nano-scale cracks at high strain and during cyclic loading. The resistance to cracks
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21 enhances the electrical performance in bending and cyclic loading. The results of both sharp
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23 bending and cycling of microfibers show that crosslinked HA/SWCNT microfibers are superb
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25 candidates for operation as actuators, which requires exposure to such severe and repeated
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27 loading conditions.
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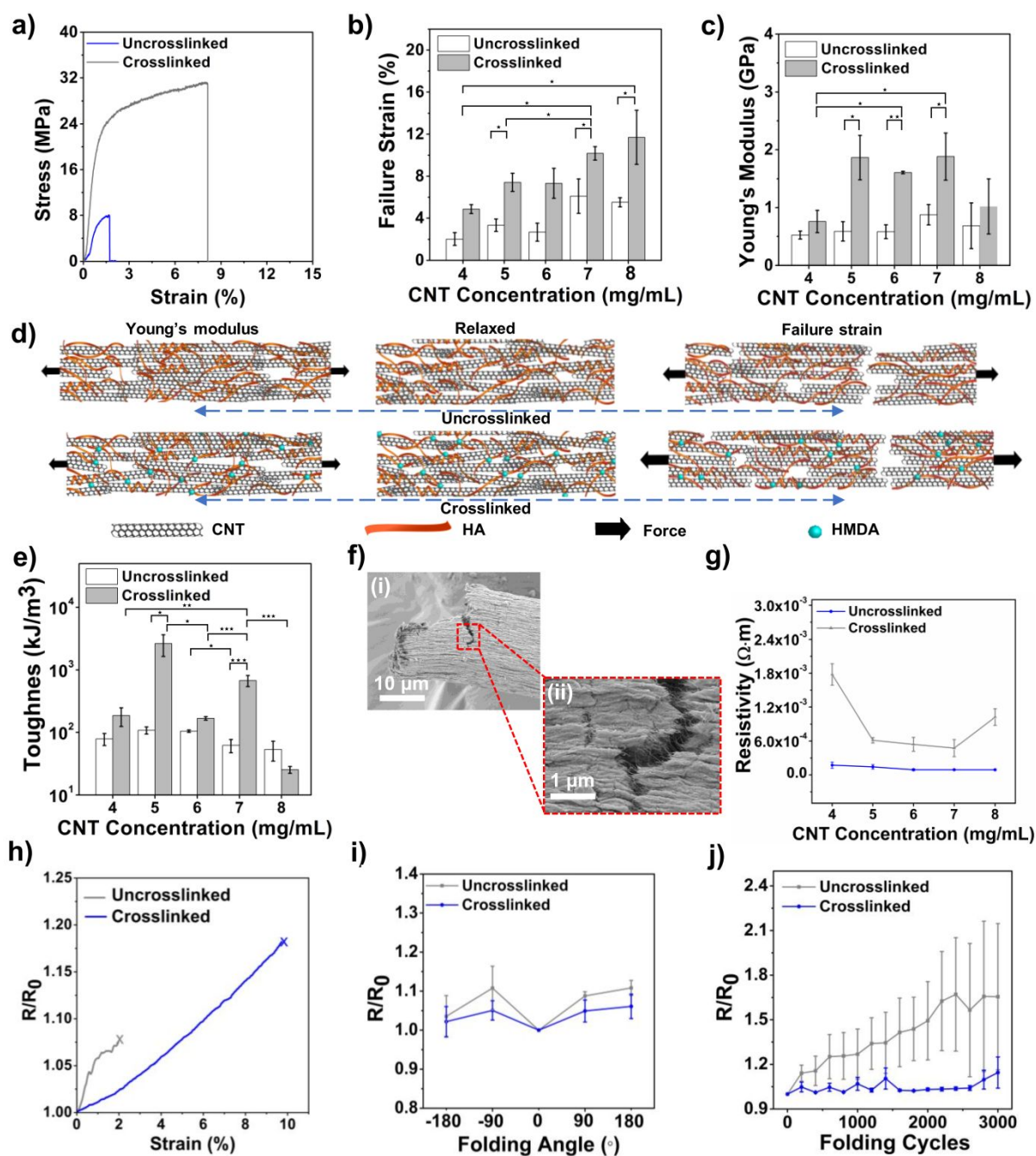


Figure 3. Mechanical and electrical properties of HA/SWCNT microfibers. a) Stress-strain curves at 6 mg/mL SWCNT concentration, b) Failure strain, and c) Young's modulus of uncrosslinked and crosslinked swollen HA/SWCNT microfibers as a function of SWCNT concentration. d) Schematic illustration of the mechanism of deformation of HA/SWCNT microfibers under tensile stress for uncrosslinked (top row) and crosslinked (bottom row) cases in the linear region for measurement of Young's modulus (left) and up to the point of fracture for measurement of failure strain (right). e) Toughness of uncrosslinked and

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3 crosslinked HA/SWCNT microfibers as a function of SWCNT concentration. f) SEM images
4 of the fractured cross-section of an HA/SWCNT microfiber with 7 mg/mL SWCNT
5 concentration after tensile testing under wet condition at (i) low and (ii) high magnifications.
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8 g) Resistivity of uncrosslinked and crosslinked HA/SWCNT microfibers with different
9 SWCNT concentrations. h) Electrical resistance of HA/SWCNT microfibers with 7 mg/mL
10 SWCNT concentration normalized to the original resistance under uniaxial strain. i) Effect of
11 bending on the resistance of HA/SWCNT microfibers with 7 mg/mL SWCNT concentration..
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14 j) Stability of the electrical resistance of the HA/SWCNT microfibers with 7 mg/mL SWCNT
15 concentration under 3000 folding-unfolding cycles. Results are presented as means \pm standard
16 deviations ($n = 3$; $*p < 0.05$, $**p < 0.01$, and $***p < 0.001$).
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30 Evaluation of the electroactivity of the HA/SWCNT microfibers through cyclic
31 voltammetry (CV) is critical for understanding their performance as electrochemical actuators.
32 Typical cyclic voltammogram (CV curve) of the investigated HA/SWCNT microfibers in the
33 DPBS (pH 7.4) at different rates from 25 to 100 mV/s are presented in Figure 4a. The
34 rectangular shape of the CV curves reveals the absence of faradic processes and the fact that
35 high electrical conductivity is maintained when the HA/SWCNT microfibers are stimulated
36 by voltage between -1 V and $+1$ V vs Ag/AgCl in the DPBS. Moreover, the rectangular shape
37 of CV represents typical charging-discharging performance of HA/SWCNT microfibers due
38 to the rapid response of current to changes in potential. The HA/SWCNT microfibers showed
39 some degree of swelling after multiple scan cycles, but still maintained their structural
40 integrity, indicating good durability of fibers. The series of CVs at different scan rates (Figure
41 S11) enabled calculation of electrochemical capacitance as high as 76.2 F/g for the
42 HA/SWCNT microfibers, which is considerably higher than that of previous biomolecule-
43 CNT hybrid fibers.²⁹ Although crosslinking reduced electrical conductivity, it has no
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3 significant effect on capacitance (Figure 4b). As CV is dominated by the double-layer
4 capacitance, the electrochemical capacitance is directly related to porosity and the surface
5 area of the materials for the adsorption of ions.⁴⁷ Therefore, higher resistance and larger
6 surface area counteract each other and cause capacitance to remain unchanged with
7 crosslinking. SWCNT concentration also did not cause a remarkable trend in capacitance,
8 though 7 mg/mL produces microfibers with slightly higher capacitance than the other
9 SWCNT concentrations (Figure 4b). The measured capacitance is excellent in the DPBS, for
10 both uncrosslinked and crosslinked microfibers, compared to other biomolecule-CNT hybrid
11 microfibers.²⁸ Large surface area of well-distributed HA-wrapped SWCNTs is probably the
12 most prominent factor affecting the double-layer capacitance and the resultant CV curves.
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26 The actuation behavior of the HA/SWCNT microfibers with 7 mg/mL SWCNT
27 concentration was determined during cycling voltammetry under a 4 mN preload (Figure 4c).
28 The HA/SWCNT microfibers expanded when they were negatively charged to -1 V and
29 contracted when they were subsequently charged positively to +1 V in the DPBS during
30 cycling voltammetry (Figure 4c, d). The final strain remained positive with reference to the
31 undeformed initial state during the entire cycle. Carbon nanotube fibers exhibit
32 electrochemical actuation when electrically charged in an electrolyte. Such actuations occur
33 via two mechanisms: (1) quantum mechanics effect, which works by a change in the length of
34 C-C bonds upon injection of electrons or holes, and (2) double layer electrostatic effect,
35 which is due to accumulation of ions at the electrode-electrolyte interface.^{27,48,49} The extent of
36 the effect of each of the deformation mechanisms in the total actuation strain depends on
37 several factors such as electrode structure, electrolyte, and voltage range.^{27,49} While
38 application of negative potential leads to electron injection to the fiber and consequently
39 positive strain, positive potential could cause different behaviors; both expansion and
40 contraction as the result of positive potential have been observed in the case of CNT.^{49,50} Here,
41 a combination of both double layer and quantum mechanics effects appear to play a role in the
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3 actuation mechanism (Figure 4d). If the double layer was the only influential factor, the larger
4 size of Cl^- anions compared to Na^+ cations should have led to larger strain in the application
5 of the positive potential and if quantum mechanics was the only effect, contraction must have
6 occurred during positive charging. We speculate that the double layer effect did not allow for
7 any contraction of the fiber upon injection of positive charge. In addition to the contribution
8 of SWCNTs in the actuation behavior, HA acts like a surfactant to produce well-dispersed
9 aqueous SWCNT solutions, and functions as an ion-conducting binder between the SWCNTs,
10 hence improving the capacitance and actuation behavior (Figure 4d). Crosslinking
11 dramatically enhanced the recoverability of strain upon application of positive charge; the
12 strain of 0.05 in the DPBS upon application of $\pm 1\text{V}$ potential was almost fully recovered in
13 several cycles while residual strain in each cycle accumulated in the uncrosslinked actuator
14 and produced a creep-like behavior (Figure 4e). Improved elasticity due to crosslinking is in
15 agreement with the enhanced mechanical performance of microfibers especially the higher
16 Young's modulus as shown in Figure 3.

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35 We further investigated the actuation behavior of the crosslinked microfibers as a function
36 of HA/SWCNT concentration in the spinning solution (Figure 4f, g). Actuation strain ranged
37 from 0.04-0.09%, with a relatively uniform trend with the change of the composition of the
38 spinning solution. SWCNT concentration of 7 mg/mL was the only exception with the highest
39 strain, consistent with the measured highest capacitance (Figure 4b), due to the optimum level
40 of SWCNT concentration to produce highest electrical conductivity. Thus, the crosslinked
41 HA/SWCNT microfibers made of spinning solutions containing 7 mg/mL SWCNT is
42 determined as the best electromechanical actuator in the DPBS among those tested,
43 considering the electrical conductivity, mechanical properties, and actuation behavior. While
44 the potential scan rate of 25 and 50 mV/s resulted in similarly excellent actuation response, an
45 increase to 100 mV/s produced a significantly lower strain, due to the limit on the speed of
46 response of the actuators (Figure 4h). The investigation of actuation performance as a

function of scan rate sheds light on the requirement of potential scan rate in the applications requiring a specified magnitude of actuation strain; a scan rate of 50 mV/s or lower is needed for a strain of 0.06% or higher.

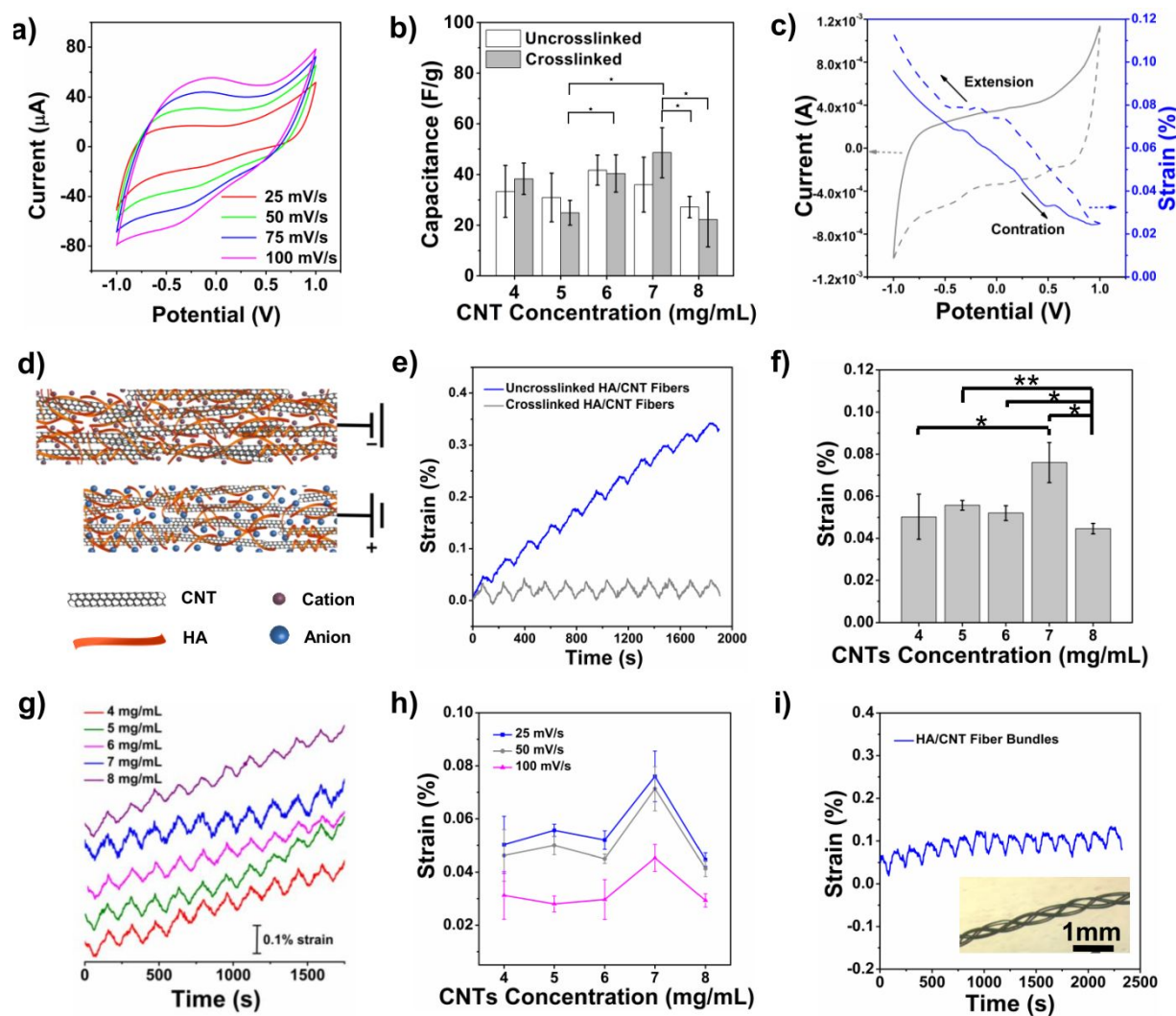


Figure 4. CV and actuation behavior of HA/SWCNT microfibers. a) Typical CV curves of the crosslinked HA/SWCNT microfibers with 7 mg/mL SWCNT concentration at different scan rates in the DPBS as electrolyte. b) Electrochemical behavior of uncrosslinked and crosslinked HA/SWCNT microfibers as a function of SWCNT concentrations. c) Strain versus potential (blue color) for crosslinked HA/SWCNT microfibers with 7 mg/mL SWCNT concentration in the DPBS during cycling voltammetry (black color) (between +1 V and -1 V

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3 versus Ag/AgCl, scan rate: 25 mV/s, electrolyte: DPBS, applied load: 4 mN. The microfibers
4 show contraction (blue solid line) and extension (blue dotted line) under oxidation (black
5 solid line) and reduction (black dotted line) state, respectively. d) Schematic illustration of the
6 actuation mechanism of an HA/SWCNT microfiber. e) Strain versus time for uncrosslinked
7 and crosslinked HA/SWCNT microfibers with 7 mg/mL SWCNT concentration during CV. f)
8 Actuation strain of crosslinked HA/SWCNT microfibers during cycling voltammetry as a
9 function of SWCNT concentration. g) Actuation strain of crosslinked HA/SWCNT
10 microfibers with different SWCNT concentrations as a function of time. h) Actuation strain of
11 crosslinked HA/SWCNT microfibers as a function of SWCNT concentration at different scan
12 rates. i) Actuation behavior of HA/SWCNT microfiber bundles with 7 mg/mL SWCNT
13 concentration and an optical image in the inset. Results are presented as means \pm standard
14 deviations ($n = 3$; $*p < 0.05$, $**p < 0.01$, and $***p < 0.001$).

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35 Tough microfibers are excellent candidates for production of macroscale yarns and sheets
36 through textile techniques such as braiding, weaving, and knitting. Toughness is critical as it
37 renders them resistant to tears and material failure. Macroscale fabrics made of nano-
38 bioactuators are suitable for biomedical applications such as tissue engineering and movable
39 devices in the human body. They are also potentially applicable to supercapacitors and
40 flexible electromechanical devices. For a proof-of-concept demonstration of fabrication of
41 such macroscale actuators, we prepared a bundle of 6 optimally made microactuators by
42 manual braiding (Figure 4i). Braiding did not adversely affect the actuation behavior; the yarn
43 showed stable 0.05% strain (Figure 4i), similar to the case of a single microfiber. The stiffness
44 of the yarn, however, is expected to be proportional to the number of used fibers, which will
45 provide the possibility of applying larger forces with the use of more fibers in a specified
46 direction. Thus, these HA/SWCNT microfibers are capable of operating as efficient

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3 macroscale electromechanical actuators in the DPBS under low voltage due to their excellent
4 mechanical properties, stable electrical performance, and electrochemical efficacy of the
5 fibers.
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10 To examine the safety of the fabricated microfibers in the body, we first investigated *in*
11 *vitro* cytotoxicity of the crosslinked HA/SWCNT microfibers and their applicability as tissue
12 scaffolds. NIH-3T3 fibroblast cells, which are commonly used as cells for evaluation of
13 cytotoxicity, were cultured on the braided HA/SWCNT microfibers. Cell viability was
14 examined by live/dead staining. The fluorescence microscopic images of Live/Dead staining
15 at day 1 and day 5 after cells seeding (Figure 5a, Figure S12) depict populations of mostly
16 live cells (green color) with a few dead cells (red color) on the surface of the yarns. The cells
17 aligned along the fiber twist direction and exhibited a stretched spindle shape. The
18 corresponding cell viability – the ratio of the number of live cells to the total number of cells
19 – was calculated on day 1 and day 5 of culture using ImageJ software. Cell viability remained
20 higher than 80% without a significant change from day 1 to day 5 (Figure 5b). To examine
21 cell adhesion and spreading patterns of the cells, their morphology on braided microactuators
22 was evaluated by staining of F-actin and nuclei on day 5 of culture. The fibroblasts were
23 spread on the surface of HA/SWCNT microfibers and exhibited elongated and well-
24 interconnected cellular shapes, indicating excellent cell-scaffold interactions (Figure 5c). Thus,
25 the results indicate that none of SWCNTs, HA, and the used crosslinking agents was toxic to
26 the cells. Furthermore, the HA/SWCNT microfibers formed suitable substrates to support cell
27 adhesion, spreading, retention and growth. Cell adhesion and cellular morphology are easily
28 affected by the surface roughness and the mechanical properties of the microfibers.^{32,51} For
29 instance, the roughness an indirect indication of porosity of the HA/SWCNT microfibers,
30 increased with crosslinking of HA (Figure S4), which is expected to improve cell-adhesion
31 strength. In addition, mechanical properties and surface texture are amenable via textile
32 techniques, which is undoubtedly beneficial for cells.
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3 Finally, we tested *in vivo* biocompatibility of the fabricated HA/SWCNT microfibers.
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5 Histology and immunohistology imaging of tissues surrounding the uncrosslinked and
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7 crosslinked HA/SWCNT microfibers were performed at 1 and 3 weeks after implantation in
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9 the subcutaneous tissue of mice. Hematoxylin and eosin (H&E) staining showed that a thicker
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11 tissue is formed around the crosslinked microfiber than the uncrosslinked one.
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13 Immunohistology images stained for CD68 (monocyte/macrophage, in green) and CD86 (M1
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15 macrophage, in red) revealed that a large number of monocytes/M1 macrophages were
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17 present around crosslinked HA/SWCNT microfibers at 1 week, compared to the
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19 uncrosslinked ones. However, after 3 weeks of implantation, the number of present
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21 monocytes/M1 macrophages decreased drastically, and only a few of them were detected in
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23 both uncrosslinked and crosslinked HA/SWCNT microfibers. Biochemical and biophysical
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25 cues presented by a biomaterial significantly influence the immune cells, especially
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27 macrophages, through altering their microenvironment.⁵²⁻⁵⁴ Stiffness, surface roughness, and
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29 surface chemistry of the crosslinked microfibers are different from those of uncrosslinked
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31 microfibers. All these factors could elicit the more severe early inflammatory immune
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33 response to the crosslinked microfiber. If foreign material is biocompatible, the early
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35 inflammatory response should be resolved. Therefore, the immunohistology results showing
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37 scarce monocyte/M1 macrophages at 3 weeks confirm the biocompatibility of uncrosslinked
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39 and crosslinked HA/SWCNT microactuators.
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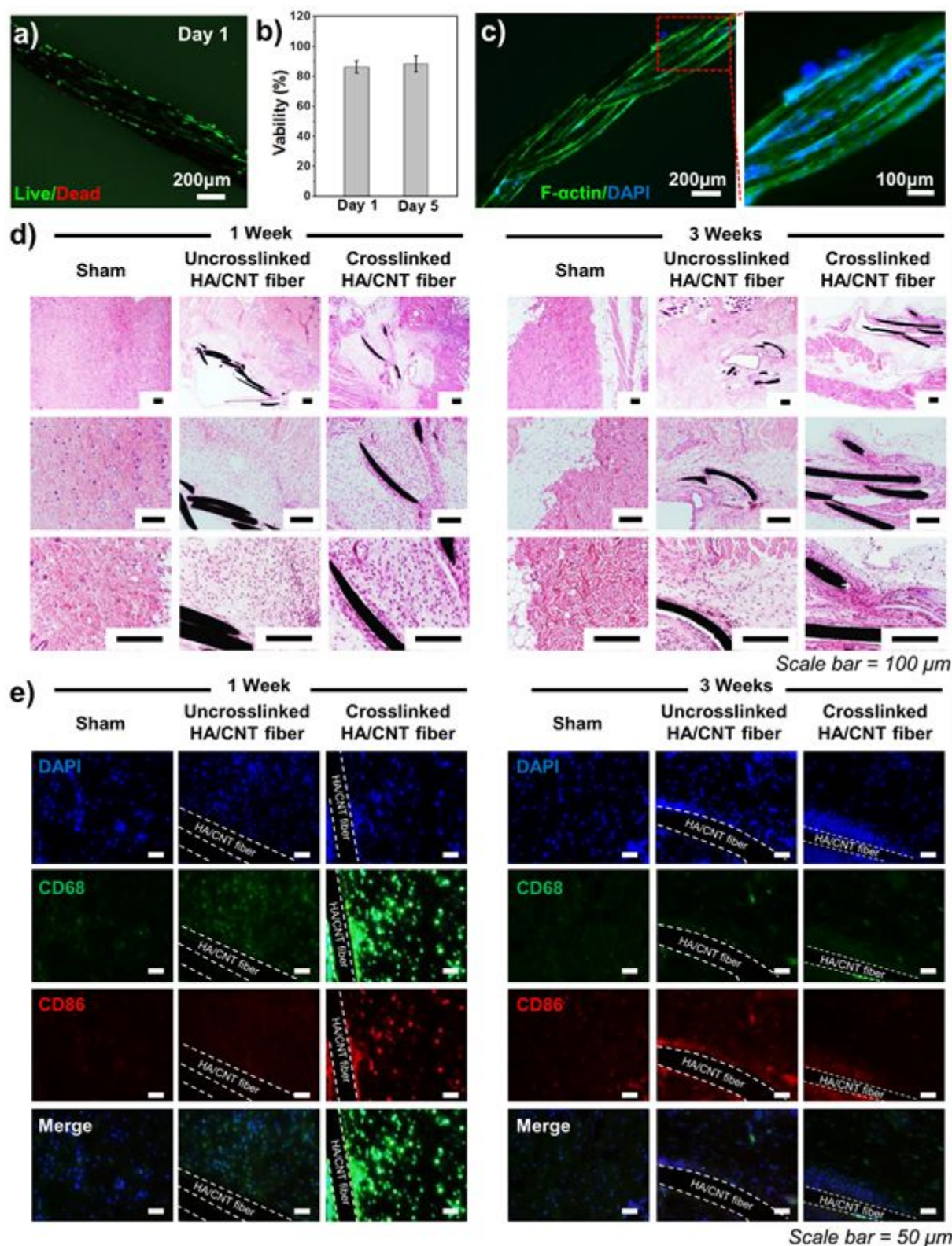


Figure 5. (a, b) Viability of NIH-3T3 fibroblasts after one day and five days of culture on the surface of crosslinked HA/SWCNT microfibers with 7 mg/mL SWCNT concentration. (c) Immunostaining of F-actin (green) and nuclei (blue) of NIH-3T3 fibroblasts after five days of

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3 culture on the surface of braided crosslinked HA/SWCNT microfibers with 7 mg/mL
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5 SWCNT concentration. (d-e) *In vivo* implantation of uncrosslinked and crosslinked
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7 HA/SWCNT microfibers with 7 mg/mL SWCNT concentration in the subcutaneous tissue of
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9 mice and staining of the tissue surrounding the implanted microfibers at 1 and 3 weeks after
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11 implantation for biocompatibility analysis; (d) H&E images and (e) immunohistology images
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13 stained for CD68 (monocyte/macrophage, in green) and CD86 (M1 macrophage, in red).
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18 **Conclusion**

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20 Biocompatible, electrically conductive and tough HA/SWCNT microfibers have been
21
22 successfully spun by a wet spinning method using HA as bio-surfactant and ion-conducting
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24 binder in the spinning solution. The HA/SWCNT microfibers presented excellent electrical
25
26 conductivity, mechanical properties and stable actuation behavior in the DPBS solution. The
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28 HA chains wrapped around SWCNTs surfaces and separated them into individual nanotubes
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30 to enhance the charge accumulated on the interface of HA/SWCNT microfibers and the
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32 electrolyte. HA had a significant contribution to the quantum mechanical and double-layer
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34 electrostatic effects responsible for the actuation strain. In particular, the crosslinking of HA
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36 offered an improvement in the mechanical properties, capacitance and the actuation stability
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38 against creep. In addition, the effects of CNT concentrations on mechanical, conductivity,
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40 electrochemical properties and actuation behavior of uncrosslinked and crosslinked
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42 HA/SWCNT microfibers were comprehensively investigated. The crosslinked HA/SWCNT
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44 microfibers with 7mg/mL SWCNT concentration were determined to possess optimum
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46 mechanical, electrical, and actuation properties. Furthermore, we were able to weave the
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48 microfibers into bundles, which showed an actuation strain of 0.05% in the DPBS as
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50 electrolyte under 4 mN preload. *In vitro* cytocompatibility and *in vivo* biocompatibility
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52 experiments were carried out, and showed that the fabricated microactuators are applicable in
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54 biomedical areas. Overall, the HA/SWCNT microfibers and bundles exhibit excellent
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3 mechanical properties, stable electrical conductivity, good electrochemical and actuation
4 behavior and, hence, prove to be promising materials for implantable microactuators and
5 flexible electronic devices in biomedical applications.
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10 11 **ASSOCIATED CONTENT**

12 13 14 15 **Supporting Information.**

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19 The Supporting Information is available free of charge on the ACS Publications website at
20
21 DOI:
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24
25 The SEM and TEM images of well dispersed HA/SWCNT solutions with 7 mg/mL
26 SWCNTs; Chemical modification sites in HA and the schematic representations of HA
27 crosslinked with HMDA after activation using EDC and HOBt; FTIR spectra of
28 SWCNTs, uncrosslinked and crosslinked HA/SWCNT microfibers; 3D topography of
29 uncrosslinked and crosslinked HA/CNTs microfiebrs with 7 mg/mL SWCNT
30 concentration obtained using AFM; Tensile strength of uncrosslinked and crosslinked
31 swollen HA/SWCNT microfibers as a function of SWCNT concentration; Failure strain
32 of uncrosslinked and crosslinked swollen HA/SWCNT microfibers as a function of
33 SWCNT concentration; SEM images of well dispersed HA/SWCNT solutions with 4
34 mg/mL and 7 mg/mL SWCNTs; Micrographs and SEM of HA/SWCNT dispersion with
35 different SWCNT concentrations; Schematic illustration of the HA/SWCNT microfibers
36 on the paper frame with different bending angles; Schematic illustration of the specimen
37 (bottom), photographs of the fibers being tested in a tensile tester at rest (left) and
38 maximum strain (right), and the corresponding load-displacement curve (middle); Cyclic
39 voltammetry outcome of the HA/SWCNT microfibers with 7 mg/mL SWCNT
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3 concentration: current vs. scan rate; Viability of NIH-3T3 fibroblasts after five days of
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5 culture on the surface of HA/SWCNT microfibers with 7 mg/mL SWCNT concentration;
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28 29 30 **Author Contributions**

31
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35 The manuscript was written through contributions of all authors. All authors have given
36 approval to the final version of the manuscript. ‡These authors contributed equally to this
37 work. *These authors contributed equally as corresponding authors to this work.
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43 44 **Notes**

45
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Table of Contents/Abstract Graphic

